

Modification of Electrical and Optical Properties by Incorporating Mn, Ta and Nb Dopants into TiO₂-Based Thin Layer Utilizing Powder-Based Physical Vapor Deposition (PPVD) Technique

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Received: August 2024

Revised: February 2025

Accepted: March 2025

DOI: 10.22068/ijmse.3707

Abstract: Powder-based Physical Vapor Deposition (PPVD) was utilized to deposit doped TiO₂ thin layers to modify electronic and optical properties. The modification was performed using several dopants (MnO₂, Ta₂O₅, Nb₂O₅) at different concentrations (0.05 and 0.1 mol%), respectively. The structural characterization by FESEM revealed that the size of the grain varied with regard to the dopants. The sample doped at a lower concentration demonstrated a larger crystallite size than the sample doped at a higher concentration. This trend is consistent with the measured grain size of the doped thin layer samples. The nonlinearity coefficient (α) and breakdown voltage (at lower ranges) were enhanced as the dopant concentration in the TiO₂ lattice increased due to grain size reduction. The optical properties of the doped TiO₂ thin layers concerning energy bandgap demonstrated an enhancement trend with the addition of the dopant, as revealed by UV-Vis reflectance analysis. The enhancement of electrical and optical properties is attributed to forming a barrier layer surrounding the grains, which increased the conductivity of the doped TiO₂ thin layers sample. This study demonstrates the feasibility of the PPVD method in producing a dense, thin layer structure for potential applications in optical and electrical sectors.

Keywords: Titanium dioxide, Powder physical vapor deposition, Breakdown voltage, Nonlinear coefficient, Energy bandgap, Adhesion strength.

1. INTRODUCTION

Titanium dioxide (TiO₂) has rapidly emerged as a widely studied metal oxide for photocatalyst application. Applications of TiO₂ photocatalysts include water treatment and organic pollutant degradation [1-3], air purification [4, 5], self-cleaning surfaces [6-8], carbon dioxide (CO₂) conversion to hydrocarbon fuels [9, 10], as well as hydrogen production by water splitting [11, 12]. TiO₂ offers several advantages: outstanding biocompatibility, low cost, non-toxicity, stable physical and chemical properties, and high availability. However, TiO₂ has been extensively researched to enhance its usefulness and efficiency [13, 14]. The relatively large band gap (3.0 eV in the rutile phase and 3.2 eV in the anatase phase) limits their photoactivity, which can be activated with the presence of ultraviolet (UV) light only [15]. As a result, this situation reduces its efficiency in utilizing solar irradiation since only 5% of the solar spectrum comprises UV light [16].

Thus, a few strategies have been attempted to modify the band gap structure, contributing to enhanced photoactivity. Generally, the research conducted focuses on finding solutions with low-cost, environment friendly, and excellent visible light driven photocatalytic activity [17]. The key to expanding the photoactivity range of TiO₂ relies on the modification of their defect chemistry through doping strategy, which in return shifts the absorption range of TiO₂ towards the visible light spectrum [18, 19]. Doping strategy is an extensively explored technique in regards to the TiO₂ modification. There are four types of TiO₂ dopant, listed as the self-doping with reduced Ti³⁺, nonmetal dopant, metal dopant, and co-dopant [20]. Given the development of TiO₂ as a photocatalyst, doping is reported together with the crystal growth, shape control, and surface modification to achieve an optimized photo response activity [21-23].

In the semiconductor-related studies, the doping process is also employed to control the formation

of Schottky barrier, which contributes to the electrical nonlinearity. This electrical nonlinearity would be highly beneficial for further applications as a voltage surge protector, which requires the high nonlinear properties [24, 25]. The diffusion of dopant ions (Ca^{2+}) into the TiO_2 lattice and occupying the Ti^{4+} site subsequently produces two electrons [26]. As a result, one free oxygen vacancy is produced to create the electric charge balance. The larger the Ca^{2+} doping concentration, the higher the oxygen vacancies. These enhanced oxygen vacancies will improve the electron movement, increasing grain conductivity. The relatively larger ionic radius and lower valence of Ca^{2+} compared to Ti^{4+} attributes to the lower solubility of Ca^{2+} within the TiO_2 lattice. Accordingly, the excess Ca^{2+} will segregate at the grain boundary, decreasing the elastic strain energy and enhancing the resistivity between the grain boundaries. This dopant segregation phenomenon also reduces the crystallite sizes and increases the TiO_2 rutile phase presence, which contributes to the high stability of TiO_2 photocatalytic activity [27]. Doping by using aluminum (Al), copper (Cu), molybdenum (Mo), and tungsten (W) leads to the narrowing of the band gap, which subsequently shifts the photoactivity towards the visible light spectrum [28]. These dopant ions are introduced into the TiO_2 lattice, presenting a localized band near the valence band that reduces the band gap energy. Oxygen vacancies increase, providing donor states below the conduction band (CB). This results in the enhancement of photocatalytic reaction [29]. This phenomenon on the modified band gap structure is also beneficial for the wettability properties of TiO_2 -based thin layers for anti-fogging and self-cleaning applications. TiO_2 comprises of Ti^{4+} and O^{2-} ions. When the TiO_2 -based thin layer is exposed to ultraviolet light, electrons from the valence band (VB) are promoted to the CB, leaving a positively charged hole. The Ti^{4+} ions are reduced to Ti^{3+} , and the oxygen atoms are ejected, contributing to the formation of oxygen vacancies. The water molecules (H_2O) will occupy these oxygen vacancies, resulting in the absorbed OH. This phenomenon will elevate the hydrophilicity of the TiO_2 surface to superhydrophilicity, resulting in improved wettability and anti-fogging capabilities [30]. However, this photoactivity is highly dependent on the presence of UV, which was previously

mentioned as one of the limitations of TiO_2 .

Thus, doping plays an essential role in improving optical and electrical characteristics. Careful consideration must be given when selecting the dopant's type and concentration. Through this research, the behavior of the TiO_2 -based thin layer was studied as a function of dopants (Mn_2O_3 , Ta_2O_5 , Nb_2O_5) with two different concentrations (0.05 and 0.10 mol%) added into the lattice structure. The structural, compositional, optical, and electrical behavior concerning nonlinearity and voltage breakdown is evaluated in detail. Furthermore, the mechanical strength of the deposited thin layer in terms of their adhesion strength has also been evaluated.

2. EXPERIMENTAL PROCEDURES

The schematic structure of the thin layer varistor of this research is presented in Figure 1. The doped TiO_2 -based thin layer was deposited as a single layer on the silicon wafer (1 0 0).



Fig. 1. The schematic structure of the TiO_2 based thin film varistor

2.1. Substrate and Target Preparation

A diamond tip cutter cut a polished p-type silicon wafer with (1 0 0) orientations into small coupons (15 mm X 15 mm). Subsequently, the small coupons were then ultrasonically cleaned in the distilled water and ethanol bath for 20 minutes. This cleaning was done following the cutting process to eliminate the grease and contaminants. These unwanted contaminants must be removed before deposition to ensure the direct adhesion of the sputtered doped TiO_2 target on the silicon substrate. The TiO_2 powder (Sigma Aldrich, US) was mixed with respective dopant powder (Mn_2O_3 , Ta_2O_5 , or Nb_2O_5) (Sigma Aldrich, US) at respective weights to produce the 99.5 mol% and 99.0 mol% composition of TiO_2 to the dopant. The details of the dopant composition in TiO_2 are tabulated in Table 1. The TiO_2 powder of 300 mesh was mixed before the deposition process using the planetary ball milling machine (Retsch PM 100) for 3 hours with the speed set at 300 rpm. This mixing step ensures the uniform distribution and homogenous mixing of TiO_2 and dopant powder.

Table 1. Details on the type and concentration of dopant in TiO₂

Sample	Designation	Composition
Mn _{0.05}	A1	0.05 mol% MnO ₂ + 99.5 mol% TiO ₂
Mn _{0.10}	A2	0.10 mol% MnO ₂ + 99.0 mol% TiO ₂
Ta _{0.05}	B1	0.05 mol% Ta ₂ O ₅ + 99.5 mol% TiO ₂
Ta _{0.10}	B2	0.10 mol% Ta ₂ O ₅ + 99.0 mol% TiO ₂
Nb _{0.05}	C1	0.05 mol% Nb ₂ O ₅ + 99.5 mol% TiO ₂
Nb _{0.10}	C2	0.10 mol% Nb ₂ O ₅ + 99.0 mol% TiO ₂

The doping of the TiO₂ takes place during the deposition process, in which the powder target is exposed to a high temperature with the plasma generated in the chamber.

2.2. Deposition Process

The deposition was carried out in an unconventional custom-made powder magnetron sputtering system. The powder mixture of TiO₂ and its respective dopants was weighed at approximately 45 g and carefully patted on the target holder of around 8 cm in diameter. The powders were levelled to get all contained in the holder. A cut of the silicon wafer was nicely placed above the target with the distance of around 8 cm. After placing the powder target and the substrate, the chamber was closed and screwed tightly to reduce any air leaking. The evacuation was started with a rough pump and followed with a turbo molecular pump reaching a low vacuum of around 4×10^{-3} Pa to ensure that the sputtered atoms can travel without colliding with other gas molecules. After that, Argon gas was purged into the chamber. The Argon gas volume was set at 25 sccm. Once the gas was stable at this amount, the radio frequency generator was increased to 200 W and adjusted to get a consistent plasma density. At this moment, the working pressure was obtained at around 0.5 Pa. For all experiments, RF power, Argon gas flow and deposition time were kept constant with 200 W, 25 sccm and 3 hours, respectively, as shown in Table 2.

Table 2. The process parameter of the PPVD technique

Parameter	Value
RF power (W)	200
Deposition time (hour)	3
Argon gas flow (sccm)	25.0

The variable manipulated was the amount of dopant composition, as shown in Table 1. Once the deposition time was over, the RF generator was shut down, and the Nitrogen gas was inserted

to start chamber ventilation. After the chamber had reached a ventilation state, the chamber section was opened, and the substrate that had been deposited was taken out and safely placed in the plastic box.

2.3. Coating Characterization

2.3.1. Structural and phase composition

X-ray diffraction (XRD, D/Max-2200) with CuK_α radiation was used to analyse the crystal phase of the thin layer samples. From the XRD spectrum obtained, the crystallite size was calculated by implementing the Scherrer equation as follows;

$$D = \frac{K\lambda}{\beta \cos \theta} \quad (\text{Equation 2.1})$$

Where D is the crystallite size (nm), K is the Scherrer constant, usually 0.94 for spherical crystallites with cubic symmetry, λ is the X-ray wavelength, CuK_α = 1.54178 Å, β is the line broadening at full width half maximum (FWHM) in radians and θ is the Bragg's angle in degree, half of 2θ . The diffraction patterns were recorded in the diffraction angles 2θ , ranging from 20° to 70°. Then, the crystal phase of the deposited thin layer samples was determined from the diffraction patterns.

2.3.2. Microstructure and elemental distribution

The thin layer varistor microstructure and morphology were observed via Field Emission Scanning Electron Microscopy (FESEM) (ZEISS SIGMA 300 VP Microscopy, Germany). The elemental composition and distribution throughout the thin layer samples were identified from the Energy Dispersive X-Ray Analysis (EDS) analysis.

2.3.3. Mechanical properties

The adhesion strength of the thin layer evaluated the mechanical properties of the deposited thin layer. Micro scratch testing was done by applying a linearly increasing load from 0 to 2500 mN along a 1000 μ m scratch length. The scratch track was observed using the optical microscope to determine the failure mode of the coating. The

load that causes a coating delamination defines the coating's critical load (LC).

2.3.4. Electrical properties

The current-voltage (I-V) curve was measured using a Keithley Electrometer (4200 SCS). Silver electrodes were sputtered on both ceramic surfaces to evaluate electrical properties. Applied voltage ranging from -10 V to 10 V with 0.05 step size was set on the electrometer before the measurement. Given the nonlinear coefficient (α) and breakdown voltage (V_B), the obtained I-V curve was further analysed for the electrical performance evaluation. The α and V_B were calculated according to Equations 2.2 and 2.3.

$$\alpha = \frac{\log(I_2/I_1)}{\log(V_2/V_1)} \quad (\text{Equation 2.2})$$

V_1 and V_2 are the voltages at the currents I_1 and I_2 , respectively.

$$V_B = nv_B \quad (\text{Equation 2.3})$$

Where v_B is the voltage barrier at a grain boundary. This measured value was utilized to evaluate the electrical performance of doped thin layer samples.

2.3.5. Optical properties

The optical behaviour of the doped TiO₂ thin layer samples was evaluated using the Ultraviolet-Visible Spectroscopy (UV-Vis) analysis. The reflectance against wavelength from UV-Vis raw data is fully utilized to obtain the energy bandgap (E_G) value. The optical reflectance coefficient ($F(R)$) was calculated according to Equation 2.4.

$$F(R) = \frac{K}{S} \quad (\text{Equation 2.4})$$

Where K and S are the absorption and scattering coefficients, respectively. The photon energy ($h\nu$) was further calculated from the relationship of frequency (ν) to the light's speed (c) and wavelength (λ) as follows;

$$h\nu = \frac{h}{2\pi} (2\pi\nu) = hf = \frac{hc}{\lambda} \quad (\text{Equation 2.5})$$

where h is the Planck's constant ($h = 6.62601 \times 10^{-34}$ Js), $c = 2.9979 \times 10^8$ m/s, and λ is the wavelength in nm. In this study, all the calculations that obtain the E_G value are carried out using graphing and analysis software, OriginLab. The E_G of each thin layer sample was calculated from the extrapolation of linear fitted line on $(F(R)h\nu)^2$ against photon energy graph.

3. RESULTS AND DISCUSSION

3.1. Structural and Phase Composition

The XRD analysis reveals that all the samples exhibited a single phase TiO₂ rutile structure, and no secondary phases were observed. This observation is due to the complete substitution of Mn, Ta, and Nb dopant into the TiO₂ lattice during deposition. The average crystallite size obtained from the Scherrer equation is tabulated in Table 3. The trend of average crystallite size decreases with the increase in dopant concentration. The Ta_{0.10} doped TiO₂ exhibits the smallest crystallite size at 153.28 ± 13.47 nm.

Table 3. The average crystallite size of each sample

Sample	Average crystallite size (nm)
Mn _{0.05}	192.68 ± 14.64
Mn _{0.10}	189.71 ± 23.25
Ta _{0.05}	187.89 ± 30.00
Ta _{0.10}	153.28 ± 13.47
Nb _{0.05}	174.78 ± 24.41
Nb _{0.10}	164.28 ± 6.56

The XRD spectrum was analysed via X'Pert Highscore software. The spectrum shows that a similar pattern of peaks illustrates all samples. The typical XRD spectrum of all samples showed that only two significant peaks were observed along 2θ from 5° to 90° . These two peaks are confined between 68° to 70° . Figure 2 reveals the existence of these peaks. The highest one is prevalent at 69.32° , showing it as the rutile phase of TiO₂. Theoretically, the phase transition usually occurs at temperatures ranging from 600 to 700°C , contributing to the changes of anatase to rutile [31].

In this research, the deposition process was conducted in the PPVD chamber, where the magnetron was designed to primarily attract and accumulate electrons in the vicinity of the target and the substrate. Therefore, it is postulated that the high impact of atoms and molecules during the deposition process may increase the temperature of the surface layer of the substrate. It eventually raises the temperature that allows the transition of the phases.

Therefore, the original anatase phase of TiO₂ transformed to the rutile phase could be expected. Apart from the main rutile phase of TiO₂, it is hypothesised that the dopant peaks could also be observed. However, due to the capability of the XRD machine, the peak is too low to be detected and thus not significant in the illustrated spectrum.

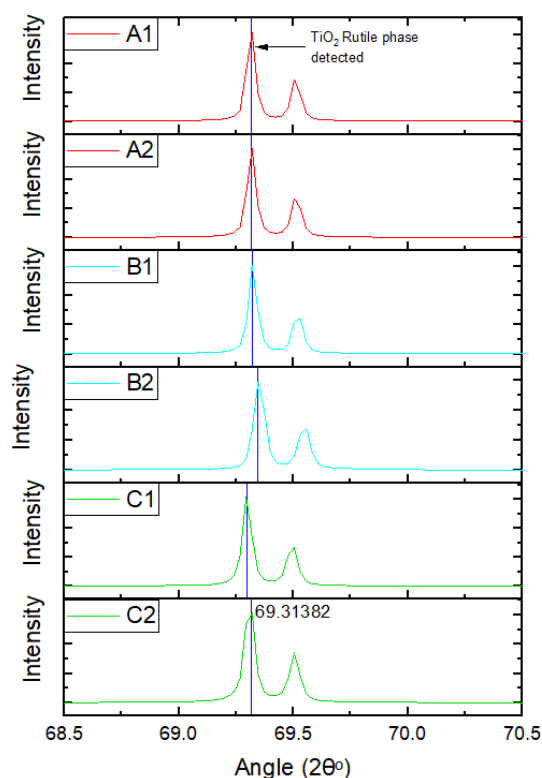


Fig. 2. The XRD spectra of the doped TiO₂ thin films

3.2. Morphological and Elemental Distribution

The FESEM image illustrates the grain size and structure differences produced with different dopants. The line intercept method is used to measure the grain size. Figure 4 illustrates the FESEM images for every sample, while Table 4 tabulates the calculated average grain size. From

the calculated values, the different concentrations significantly affect the grain size of the particle. The trend reveals that the higher dopant concentration produces smaller grains. The thin layered sample with 0.10 mol% exhibits smaller grain sizes than those with 0.05 mol% dopant concentration. The smaller the grain size, the more grain boundaries are formed, which subsequently enhances the nonlinear electrical properties of the thin layer in varistor application. An observation from previous research reveals the decrease of grain size with the addition of dopant, which in return reduces the total electrical conductivity of TiO₂ doped with ZrO₂ varistor [32, 31]. This observation is consistent with the obtained results of this study.

Further analysis by EDS confirms (as presented in Figure 4) the presence of dopant, hence proving that the mixing of two different powders, TiO₂ and dopant (MnO₂, Ta₂O₅ & Nb₂O₅), has taken place successfully and subsequently deposited on the substrate.

Table 4. The grain size average, after taking five different dimensions from the micro image of each sample

Sample	Average grain size (nm)
Mn _{0.05}	462.07 ± 33.40
Mn _{0.10}	343.01 ± 28.11
Ta _{0.05}	485.10 ± 41.75
Ta _{0.10}	391.52 ± 44.28
Nb _{0.05}	543.66 ± 50.57
Nb _{0.10}	527.35 ± 51.42

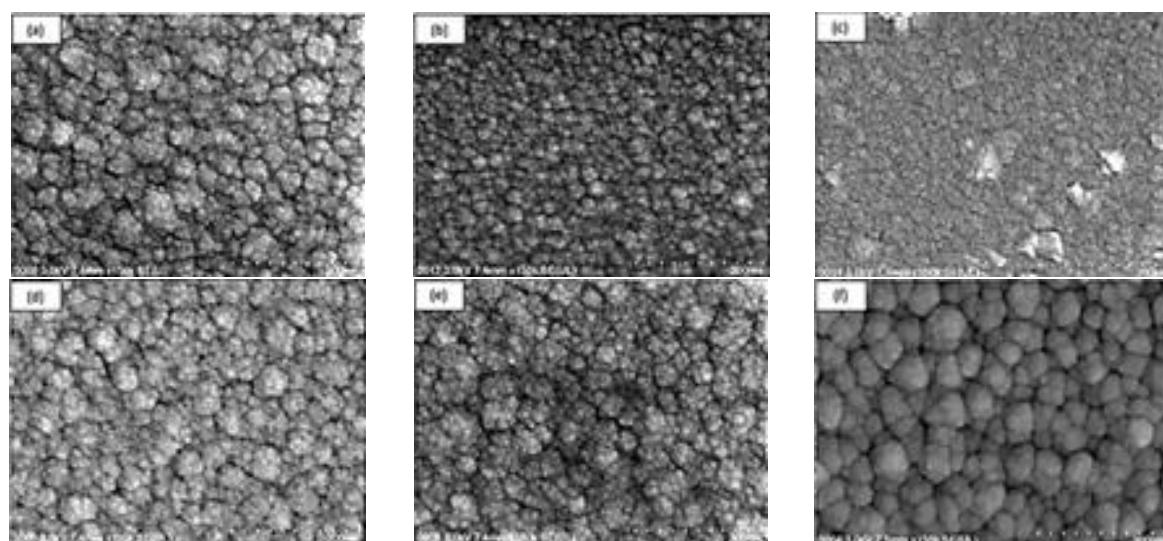


Fig. 3. The FESEM images of doped TiO₂ thin films with; a) Mn_{0.05}, b) Mn_{0.10}, c) Ta_{0.05}, d) Ta_{0.10}, e) Nb_{0.05}, and f) Nb_{0.10}

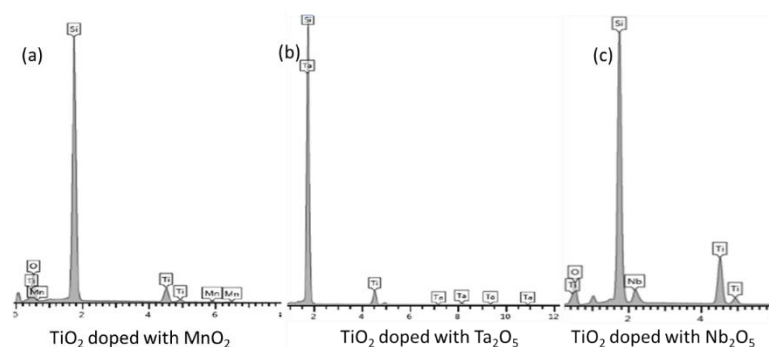


Fig. 4. EDS result of each sample

3.3. Mechanical Properties

The adhesion strength of the deposited TiO₂ ceramics layer was measured in this research to evaluate the mechanical strength of each thin layer. Generally, the properties of varistor samples were studied because of their structural, optical, and electrical behaviours only. The mechanical evaluation of the thin layer is studied in this research to evaluate the PPVD technique in developing a functional thin layer with excellent mechanical properties.

A 1000 μm scratch was produced on a typical 3-5 μm thick coated sample. The image was observed under an optical microscope. The critical load was determined at the point of coating failure, revealing the substrate underneath. The scratch test was done on three samples (Mn_{0.05}, Ta_{0.05}, and Nb_{0.05}) to evaluate the adhesion strength of the TiO₂-based thin layers. Table 5 tabulates the result of the scratch test concerning their failure length and critical load for the coating to fail.

Table 5. The adhesion strength of the TiO₂-based thin layers sample

Sample	Failure length and critical load (L_c)
Mn _{0.05}	Fails at 836.59 with load 1310.60 mN
Ta _{0.05}	Fails at 842.63 with load 1321.62 mN
Nb _{0.05}	Fails at 833.76 with load 1304.64 mN

The recorded result of the scratch test does not reflect a significant influence of dopants type on the adhesion of deposited TiO₂ thin layer. The doping strategy on the TiO₂-based thin layer does not seem to be a key factor in influencing their adhesion strength. This insignificant adhesion strength can be due to the same processing parameter of PPVD set during the deposition process.

Higher RF power will result in higher energy of

sputtered atoms on the substrate surface. The flow rate of the working Ar gas into the deposition chamber also plays a vital role by increasing the deposition rate, which subsequently influences the density and adhesion of the thin layers. However, since the RF power and Ar flow rate throughout the sample's preparation is maintained at 200 W and 25.0 sccm, the energy of sputtered atoms also does not vary. Thus, subsequently contributes to this indifferent adhesion strength of the deposited doped TiO₂ thin layers.

3.4. Electrical Properties

The I-V characteristic for all samples is illustrated in Figure 5. The nonlinear coefficient increases when the dopant concentration is increased from 0.05 to 0.1 mol%. The doping with 0.1 mol% Ta₂O₅ demonstrates a good nonlinear coefficient $\alpha = 1.56$. The varistor's VB increases with the grain size decrease, showing the increasing doping concentration. The resistivity of the TiO₂ grains increases with the increase of the doping amount due to the growing grain boundaries.

The value for the nonlinear coefficient for MnO₂ is lower than the Ta-doped varistor sample. The increase in the dopant concentration successfully contributes to improving the nonlinear coefficient. The increase in the concentration of the dopant MnO₂ could decrease the grain size [33]. In other perspectives, SEM images show that different materials produce different grain sizes. This occurred due to different ionic radii for each of the three elements. Mn²⁺, Ta⁵⁺, and Nb⁵⁺ have ionic radii of 0.07 nm, 0.064 nm and 0.065 nm, respectively. At the same time, Ti⁴⁺ has an ionic radius of 0.061 nm. All three elements have similar ionic radii that help the dopant ions dissolve into the TiO₂ lattice easily. This promotes the formation of the grain in TiO₂. However, when the dopant concentration increases, the size of

the grain starts to decrease, as demonstrated by the average grain and crystallite size results. Thus, dopant concentration plays a vital role in modifying the performance of TiO_2 samples.

The formation of the grain boundary or the depletion layers hinders the movement of the transmitted electrons. Hence, the amount of dopant increases the formation of this layer while decreasing the grain size. More barriers will be formed to hinder the electrons. The breakdown voltage is reduced as the concentration of the dopant increases. Adding this particular dopant can decrease the resistivity of a specific grain, including the breakdown voltage.

The decrease in the grain resistance promotes the formation of barriers at the grain boundaries and

simultaneously enhances the nonlinear coefficient. The ionic radius from each particular ion also affects the grain growth and the breakdown voltage. The closest ionic radius to Ti^{4+} which is Ta^{5+} and Nb^{5+} , produced lower breakdown voltage compared to Mn^{2+} , Table 5.

It can be found that the thin layer varistor with 0.1 mol% Ta_2O_5 has the best nonlinear electrical property with the highest nonlinear coefficient, α 1.56 with breakdown voltage of 0.7 Vmm^{-1} . This thin-layer varistor may benefit low voltage protection applications requiring smaller voltage clamping dimensions. The value of the nonlinear coefficient may reach its maximum and then decrease with increasing the dopant concentration.



Fig. 5. Voltage-current curves for A1, A2, B1, B2, C1, and C2 respectively

Table 6. The calculated values of nonlinear coefficient (α) and voltage breakdown (V_B) of each sample

Sample	Nonlinearity Coefficient, α	Breakdown Voltage, V_B (V)
$\text{Mn}_{0.05}$	1.0260	0.95
$\text{Mn}_{0.10}$	1.1989	0.85
$\text{Ta}_{0.05}$	1.3204	1.10
$\text{Ta}_{0.10}$	1.5679	0.70
$\text{Nb}_{0.05}$	0.7491	0.45
$\text{Nb}_{0.10}$	0.9959	0.10

This observation is attributed to the hindrance of electron movement with the decrease in grain size and an enhanced barrier layer. This phenomenon has significantly affected the electrical properties of these doped TiO₂ thin layers.

3.5. Optical Properties

The optical properties evaluation, given the reflectance spectrum obtained from UV-Vis analysis, reveals the alteration of optical bandgap energy. The Tauc plots were constructed to determine each thin layer sample's respective energy bandgap (E_G), Figure 6. The value of E_G is tabulated in the following table, Table 6.

Table 7. The E_G values of each of the doped TiO₂ thin layers

Sample	Energy bandgap, E _G
Mn _{0.05}	3.17
Mn _{0.10}	3.15
Ta _{0.05}	3.16
Ta _{0.10}	3.09
Nb _{0.05}	3.19
Nb _{0.10}	3.23

The evaluation of E_G reveals that the trend is consistent according to their grain size and electrical properties. A doped sample with 0.10 mol% Ta₂O₅ exhibits the lowest energy bandgap, indicating the effective enhancement of optical properties through the doping strategy. The

consistency of this E_G with other results demonstrated the direct correlations of structural modification, which subsequently influences the electrical and optical properties of the doped samples.

4. CONCLUSIONS

The TiO₂ thin layer doped with three different materials, MnO₂, Ta₂O₅, and Nb₂O₅, at two concentrations, 0.05 and 0.10 mol%, were successfully developed via the unconventional PVD method. The influence of the dopant type and concentration on the TiO₂ doped varistor was studied, given their structural, elemental distribution, and electrical performance characterization. The increase in dopant concentration has effectively enhanced the nonlinear coefficient, grain resistance, and energy bandgap due to the reduction of grain sizes of the lattice system. The TiO₂ varistor sample with 0.10 mol% Ta₂O₅ possesses the best electrical and structural properties. The feasibility of the unconventional PVD method to produce an electrical functioning thin layer has been demonstrated through this research.

DECLARATION OF INTERESTS

The authors declare no competing financial interests or personal relationships that influence the work reported in this paper.

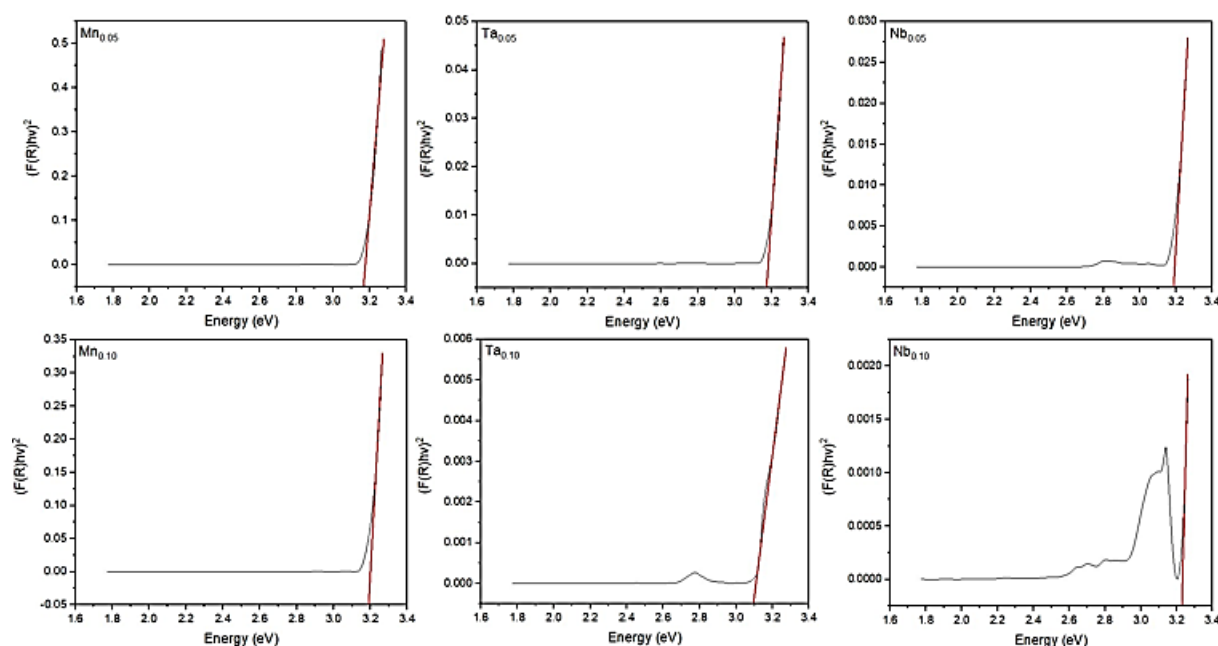


Fig. 6. Tauc plots of respective doped TiO₂ thin films

ACKNOWLEDGEMENT

The authors would like to express gratitude to the Lembaga (Penyelidikan dan Kemajuan) Perusahaan Timah, Malaysia with grant number: GA034-2023 that has partially funded this study.

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